

REBUTTAL TESTIMONY

OF

MONA ELSAID

ELECTRICAL ENGINEER

ENGINEERING DEPARTMENT

ENERGY DIVISION

ILLINOIS COMMERCE COMMISSION

ILLINOIS POWER COMPANY d/b/a AmerenIP

Docket No. 10-0079

Petition for a Certificate of Public Convenience and Necessity, pursuant to Section 8-406 of the Illinois Public Utilities Act, to construct, operate and maintain a new 345,000-volt electric transmission line in Macon County, Illinois

January 19, 2011

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1 **Introduction and Witness Qualification**

2 **Q. Please state your name and business address.**

3 A. My name is Mona Elsaid. My business address is 527 East Capitol Avenue,  
4 Springfield, Illinois 62701.

5  
6 **Q. Are you the same Mona Elsaid who previously filed direct testimony in this  
7 proceeding?**

8 A. Yes.

9  
10 **Q. Do you use acronyms in your testimony?**

11 A. Yes. Below is a list of the acronyms used along with the full terms spelled out.

- 12 • kV stands for kilovolt or thousand volts.  
13 • MW stands for megawatts or million watts. A watt is a measure of electric  
14 power that can perform useful work.

15  
16 **Q. Are there any attachments to your rebuttal testimony?**

17 A. Yes. Attachments A and B are attached to my testimony. The attachments are  
18 described as follows:

19 Attachment A, marked as ICC Staff Ex. 3.0, Attachment A, consists of one page  
20 and is a copy of an attachment (identified as “ENG 4.06, Attach 5”) to

21 AmerenIP’s responses to Staff data requests ENG 4.06.<sup>1</sup>

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<sup>1</sup> The two-page response to data request ENG 4.06 was provided as Attachment C to ICC Staff Ex. 1.0. However, the 5 attachments to said response had not been included in ICC Staff Ex. 1.0.

22 Attachment B, marked as ICC Staff Ex. 3.0, Attachment B, consists of one page  
23 and is a copy of AmerenIP Ex. 7.1.  
24

25 **Purpose and Scope**

26 **Q. What is the purpose of your rebuttal testimony in this proceeding?**

27 A. On September 23, 2010, Illinois Power Company d/b/a AmerenIP (“AmerenIP”)  
28 filed a rebuttal testimony of Mr. Curtis E. Stepanek (AmerenIP Ex. 7.0) to  
29 respond to my direct testimony (ICC Staff Ex. 1.0) regarding the need for the  
30 proposed project in this proceeding. The purpose of my rebuttal testimony is to  
31 respond to the rebuttal testimony of AmerenIP’s witness Mr. Stepanek  
32 (AmerenIP Ex. 7.0).  
33

34 **Q. What information did you review to drive a conclusion in this rebuttal  
35 testimony?**

36 A. I reviewed the rebuttal testimony of Curtis E. Stepanek (AmerenIP Ex. 7.0), a  
37 power flow diagram supporting Mr. Stepanek’s rebuttal testimony (AmerenIP Ex.  
38 7.1), and AmerenIP’s responses to Staff data requests.  
39

40 **Summary of Conclusions**

41 **Q. Please provide a summary of the conclusions you have drawn from your  
42 examination of AmerenIP’s rebuttal testimony (AmerenIP Ex. 7.0).**

43 A. Based on the information that AmerenIP provided in its rebuttal testimony and in  
44 response to Staff data requests, I conclude that the proposed transmission line is

45 needed by 2015 to comply with Ameren Transmission Planning Criteria.<sup>2</sup> The  
46 proposed transmission line should hedge against unacceptable low-voltage  
47 conditions<sup>3</sup> that might happen in the event of the outage of the Clinton to Latham  
48 345 kV transmission line and the Clinton to Goose Creek 345 kV transmission  
49 line under a quick voltage collapse scenario.

50

### 51 **The Need for the Proposed Transmission Line**

52 **Q. What did AmerenIP conclude regarding the need of the proposed project in**  
53 **its rebuttal testimony (AmerenIP Ex. 7.0)?**

54 A. Based on a revised power flow analysis of the Decatur area that shows  
55 unacceptable low-voltage levels on many distribution buses, AmerenIP  
56 concluded as indicated in its rebuttal testimony<sup>4</sup> that, in order for AmerenIP to  
57 comply with its transmission planning criteria and to avoid a voltage collapse and  
58 the consequent outage, the proposed project should be completed by 2015.

59

60 **Q. AmerenIP provided four power flow models with its original filing**  
61 **(AmerenIP Exs. 1.4-1.7). Which model did AmerenIP revise?**

62 A. AmerenIP did not revise or use AmerenIP Exs. 1.4 -1.7 to support the need of  
63 the proposed project in its rebuttal testimony (AmerenIP Ex. 7.0). AmerenIP  
64 revised its power flow model that was provided as part of its response to Staff  
65 data request ENG 4.06(d) and used the revised version to prove the need of the

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<sup>2</sup> AmerenIP Ex. 7.0, p.3, lines 55-64.

<sup>3</sup> AmerenIP voltage criteria used in identifying low voltage conditions are indicated in AmerenIP Ex. 1, pp. 9-10, lines 203-218.

<sup>4</sup> AmerenIP Ex. 7.0, pp. 21-22.

66 proposed transmission line by 2015 in its rebuttal testimony.<sup>5</sup> Both the power  
67 flow model from earlier discovery (“ENG 4.06, Attach 5”) and the power flow  
68 model provided in AmerenIP’s rebuttal testimony (AmerenIP Ex. 7.1) are  
69 attached to this testimony as Attachments A and B respectively.

70

71 **Q. What is the key difference(s) between the aforementioned power flow**  
72 **model that was provided in response to Staff data request ENG 4.06(d) and**  
73 **the model that AmerenIP provided with its rebuttal testimony (AmerenIP**  
74 **Ex. 7.1)?**

75 A. The aforementioned power flow model<sup>6</sup> that was provided as part of AmerenIP  
76 response to Staff data request ENG 4.06(d) models the Decatur area’s electric  
77 system under the following conditions:

- 78 • A load level of 620 MW by 2016;
- 79 • The outage of both the Clinton to Latham 345 kV transmission line and the  
80 Clinton to Goose Creek 345 kV transmission line;
- 81 • After the operation of the transformer load tap changers (LTC) to mitigate low  
82 voltage conditions; and
- 83 • After dropping a load of 90 MW to mitigate low voltage conditions.

84 The aforementioned model suggests that there will not be a need for the  
85 proposed project by 2016, because AmerenIP will be able to control the low  
86 voltage conditions in the Decatur area in the event of the outage of both Clinton  
87 to Latham 345 kV transmission line and the Clinton to Goose Creek 345 kV

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<sup>5</sup> AmerenIP Ex. 7.0, p. 15, lines 321-322.

<sup>6</sup> ICC Staff Ex. 3.0, Attachment A.

88 transmission line. The model also suggests that, without the proposed project,  
89 AmerenIP will stay in compliance with Ameren Transmission Planning Criteria  
90 and NERC Standards in 2016.

91 However, the new power flow model<sup>7</sup> models the Decatur area's electric system  
92 under the following conditions:

- 93 • A load level of 620 MW by 2016;
- 94 • The outage of both the Clinton to Latham 345 kV transmission line and the  
95 Clinton to Goose Creek 345 kV transmission line;
- 96 • Before the operation of the transformer load tap changers (LTC);
- 97 • No drop for any load to mitigate low voltage conditions; and
- 98 • More explicit modeling to some of the electric components (capacitors) on the  
99 underlying distribution system.<sup>8</sup>

100 In its original filing, AmerenIP provided two exhibits, AmerenIP Exs. 1.5 and 1.6,  
101 to show the Decatur area electric system after the outage of the Clinton to  
102 Latham 345 kV transmission line and the Clinton to Goose Creek 345 kV  
103 transmission line, and before and after the transformer LTCs operate, assuming  
104 a load level of 660 MW by 2013.<sup>9</sup> However, in its rebuttal testimony, AmerenIP  
105 decided to study the electric system in the Decatur area under a load level of 620  
106 MW, before the operation of the LTCs (*i.e.*, assuming that the LTCs will not  
107 operate in a timely manner),<sup>10</sup> without dropping any load to mitigate low voltage

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<sup>7</sup> ICC Staff Ex. 3.0, Attachment B.

<sup>8</sup> AmerenIP Ex. 7.0, p. 14, lines 314-317.

<sup>9</sup> AmerenIP Ex. 7.0, p. 13, lines 276-277.

<sup>10</sup> AmerenIP Ex. 7.0, p. 8, lines 166-173.

108 conditions (*i.e.*, assuming dropping a load will not be doable timely),<sup>11</sup> and with  
109 explicit modeling to electric components called capacitors, as indicated in  
110 AmerenIP Ex. 7.1.

111

112 **Q. Did AmerenIP explain why it revised its original power flow model?**

113 A. Yes. In its rebuttal testimony, AmerenIP indicated that the power flow models  
114 that are used to evaluate the transmission system do not explicitly represent the  
115 details of the distribution systems.<sup>12</sup> In addition, AmerenIP added that the model  
116 used in its initial evaluation of the Decatur area understated the exposure to  
117 voltage collapse.<sup>13</sup>

118

119 **Q. Is there any electric equipment or electric device that can be used to  
120 restore the voltage to acceptable levels?**

121 A. Yes. Transformer LTCs and voltage regulators can take the voltage to  
122 acceptable levels (up or down), but the LTCs and voltage regulators react after a  
123 certain time delay. However, AmerenIP assumes and explains that the voltage  
124 collapse may happen very quickly,<sup>14</sup> that is, before the LTCs and voltage  
125 regulators are able to react.<sup>15</sup> To support the aforementioned assumption,  
126 AmerenIP's new model<sup>16</sup> is built to represent the voltage levels before the  
127 operation of LTCs, assuming that the LTCs will not be fast enough to restore the

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<sup>11</sup> AmerenIP Ex. 7.0, p. 8, lines 174-178.

<sup>12</sup> AmerenIP Ex. 7.0, p. 13, lines 285-286.

<sup>13</sup> AmerenIP Ex. 7.0, p. 14, lines 310-312.

<sup>14</sup> AmerenIP Ex. 7.0, p. 5, lines 92-93 and p.6, lines 123-129.

<sup>15</sup> AmerenIP Ex. 7.0, p. 8, lines 166-173.

<sup>16</sup> AmerenIP Ex. 7.1.

128 voltage in the Decatur area to acceptable levels. AmerenIP also indicated that,  
129 for a fast-acting voltage collapse involving an outage of a transmission line,  
130 system operators will not be able to respond quickly enough to prevent a voltage  
131 collapse.<sup>17</sup>

132

133 **Q. Did AmerenIP specify the voltage level when the voltage collapse is**  
134 **assured?**

135 A. Yes. AmerenIP specified the voltage level when voltage collapse is assured to  
136 be 85% of the voltage original value.<sup>18</sup>

137

138 **Q. Did AmerenIP include the voltage levels under its new model (AmerenIP Ex.**  
139 **7.1)?**

140 A. Yes.<sup>19</sup> Based on those levels, it is clear that there will be two buses with voltage  
141 levels far below the 85% of their original value and many buses with  
142 unacceptable low voltage levels.

143

144 **Q. What do you conclude about the need for the proposed transmission line?**

145 A. Based on AmerenIP revised model and new assumptions, I conclude that the  
146 proposed transmission line is needed to comply with Ameren Transmission  
147 Planning Criteria. The proposed transmission line would hedge against low-  
148 voltage conditions that might happen in the event of the outage of the Clinton to

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<sup>17</sup> AmerenIP Ex. 7.0, p. 8, lines 174-178.

<sup>18</sup> AmerenIP Ex. 7.0, p. 21, line 440.

<sup>19</sup> AmerenIP Ex. 7.0, pp. 15-16.

149 Latham 345 kV transmission line and the Clinton to Goose Creek 345 kV

150 transmission line, assuming a quick voltage collapse.

151

152 **Recommendations**

153 **Q. What are your overall recommendations regarding the proposed**  
154 **transmission line?**

155 A. I recommend that the Commission grant AmerenIP a Certificate of Public  
156 Convenience and Necessity, pursuant to Section 8-406 of the Public Utilities Act  
157 (“Act”), 220 ILCS 5/8-406, and authorize AmerenIP to construct the proposed  
158 project, pursuant to Section 8-503 of the Act, 220 ILCS 5/8-503, by the year  
159 2015. I also support AmerenIP’s primary route “Route A” as the least cost and  
160 best route, as I mentioned in my direct testimony.

161

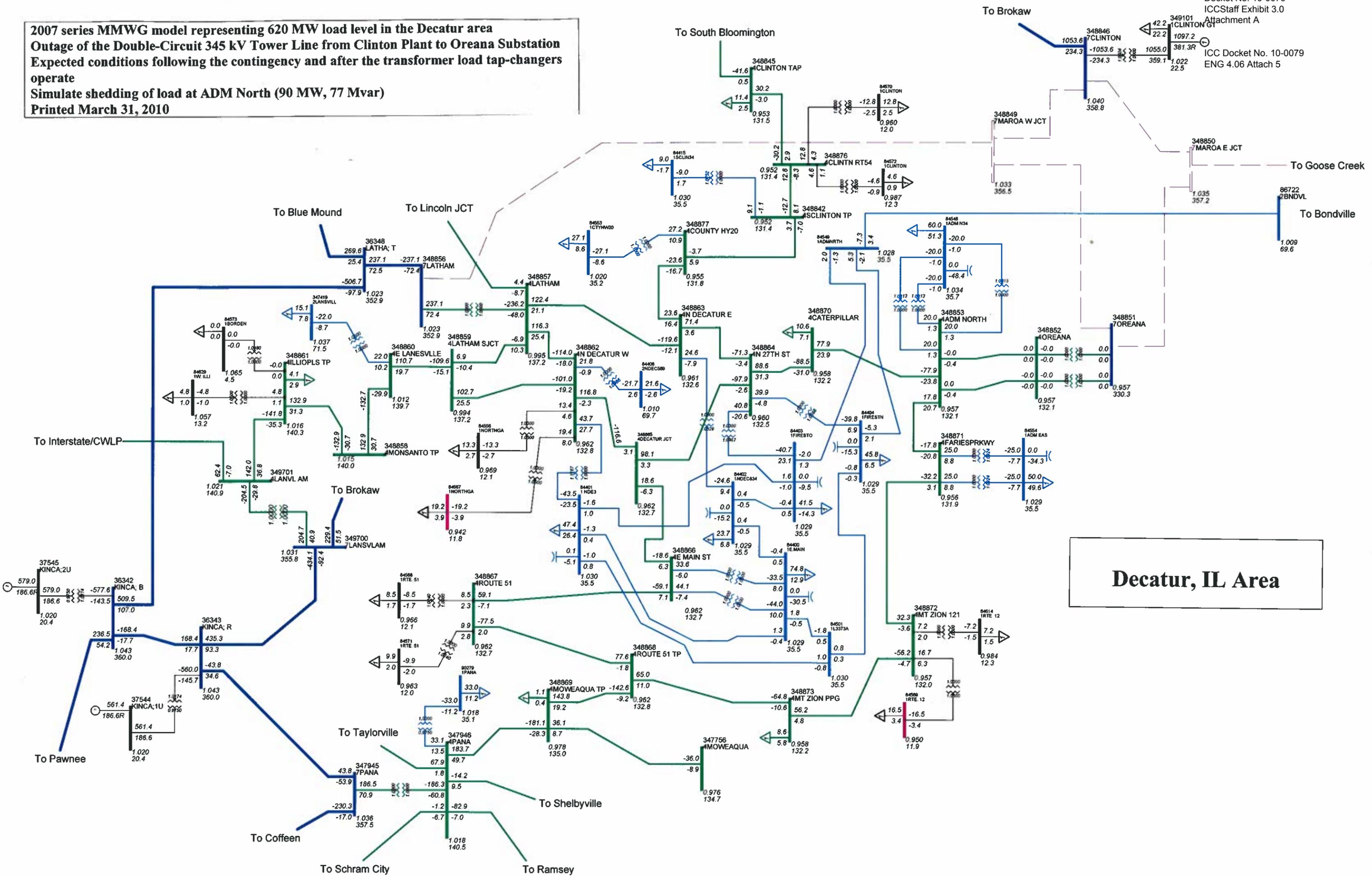
162 **Conclusion**

163 **Q. Does this conclude your rebuttal testimony?**

164 A. Yes.

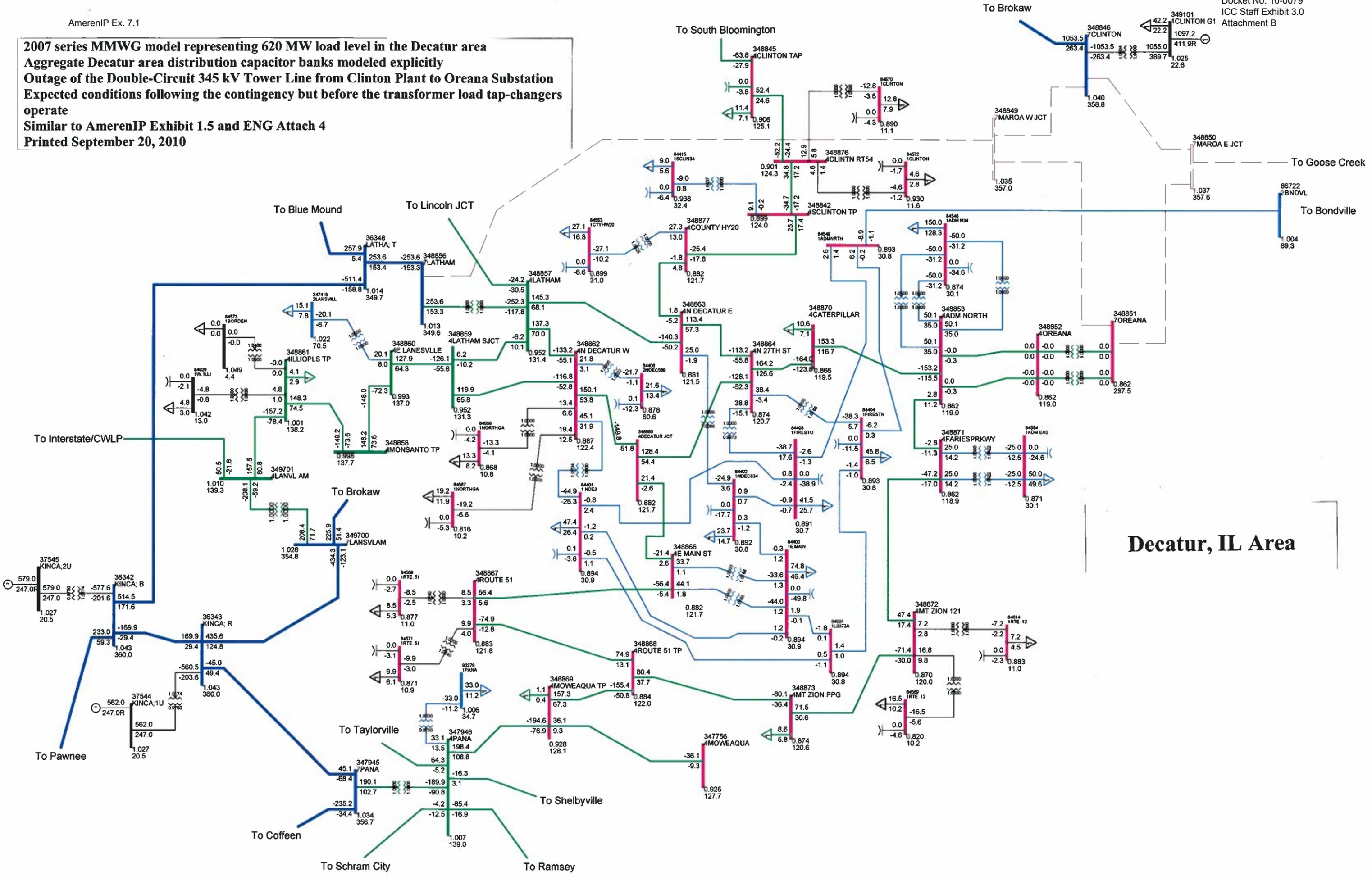
2007 series MMWG model representing 620 MW load level in the Decatur area  
 Outage of the Double-Circuit 345 kV Tower Line from Clinton Plant to Oreana Substation  
 Expected conditions following the contingency and after the transformer load tap-changers operate  
 Simulate shedding of load at ADM North (90 MW, 77 Mvar)  
 Printed March 31, 2010

Docket No. 10-0079  
 ICCStaff Exhibit 3.0  
 Attachment A  
 ICC Docket No. 10-0079  
 ENG 4.06 Attach 5



Decatur, IL Area

**2007 series MMWG model representing 620 MW load level in the Decatur area**  
**Aggregate Decatur area distribution capacitor banks modeled explicitly**  
**Outage of the Double-Circuit 345 kV Tower Line from Clinton Plant to Oreana Substation**  
**Expected conditions following the contingency but before the transformer load tap-changers operate**  
**Similar to AmerenIP Exhibit 1.5 and ENG Attach 4**  
**Printed September 20, 2010**



Decatur, IL Area